

Composite Action Between Light Steel And Concrete For Beams, Walls And Floor

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Abstract: *In this paper — The composite behaviour of steel beams and columns with concrete is well understood for hot rolled steel members and hollow steel sections, but is not properly researched for cold formed steel sections. In this case, the behaviour is affected by the relatively flexible shear connection between the steel and concrete and by local buckling of the thin steel sections. Shear connection may be in the form of mechanical connectors such as bolts or screws, or embossments or perforations rolled into the thin steel. In both cases, the shear connection may be assisted by local confinement of the concrete within the steel profiles. In this project addresses the behaviour of light steel composite beams using C-sections acting in tension and in shear with different forms of shear connection, and also the behaviour of composite columns using perforated C-sections in a form of box sections. The aim is to show to what extent composite action increases the stiffness and bending resistance of the thin C profiles in bending and compression. For composite beams, tests were performed on 0.8m, 1.1m and 1.7m span beams of approximately 150 mm depth using 100x 50x 1.2 mm C-sections as tensile reinforcement. The shorter span beams failed by shear-bond and possibly by pure shear, and some of the longer span beams failed in pure bending without end slip. The shear connectors were in the form of 4.8 mm diameter screws and 6 mm diameter bolts with double nuts, and also perforated webs with 5 lines of 5 mm wide slots. It was shown that the shear-bond strength of the perforated C-sections was over 1.2 N/mm² when expressed as a stress over the web area times the shear span. Tests were also performed on beams with side C-sections which greatly improved the shear resistance of these beams. The stiffness of the beams was analyzed by elastic theory and it was shown that the elastic stiffness of the shear connection to the perforated section is 10 N/mm/mm² area of web. This reduces to 4 N/mm/mm² for the mechanical shear connectors, partly because of the rotation of the screws and bolts at their connection to the thin web .A study will made of the application of this method of construction using perforated base and side C-sections for a beam span of 7.2m with various end conditions and it was shown to be sufficiently stiff and strong for residential loading added to the self-weight..*

Keywords: *Composite Action; C-Section; CFS-Cold Formed Steel ; Shear Connection; ABAQUS; FEA; Ansys Software*

I. INTRODUCTION

The composite behaviour of steel beams and columns with concrete is well understood for hot rolled steel members and hollow steel sections, but is not properly researched for cold formed steel sections. In this case, the behaviour is affected by the relatively flexible shear connection between the steel and concrete and by local buckling of the thin steel sections. Shear connection may be in the form of mechanical connectors such as bolts or screws, or embossments or perforations rolled into the thin steel. In both cases, the shear connection may be assisted by local confinement of the concrete within the steel profiles.

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II. RESEARCH MOTIVATIONS

The primary motivation for this project was to examine the potential for a new form of composite construction using cold formed steel sections and on-site concrete. It is important that the system must be easy to construct and should require the minimum deviation from current light steel framing construction. The benefits of composite construction would lead to improved load capacity particularly of columns and walls and should extend the span range of C sections in bending. In this project, new forms of shear connections were investigated. Perforated C-sections are used to provide a roofs and façade walls as a function of discontinuity of the web.

A special perforated C-section with semi-punched through slots in the web was provided for this research. This was first developed for use in the building facades and roofs to reduce thermal bridging but it was considered to offer the potential for a high degree of composite action.

The perforations consist of 5 parallel lines of 5 mm depth and 40 mm length of 2 mm deep partially punched slots extending over a width in a zone of 65 mm of the web of the C-section. This perforated pattern is used in both 100 mm deep and 150 mm deep C-sections. Same pattern of perforations can also be added to the web of Z sections. Figure 1-5 shows a perforated C-section and the perforation pattern. This type of perforation is considered to be an excellent form of shear connector because the concrete fills into and around the perforations.

III. LITERATURE SURVEY

[1] **Farid Abed (2019)** The main aim of this study was to evaluate the bond dependent coefficient of concrete beams reinforced with GFRP bars exposed to harsh environmental conditions of direct sunlight and seawater. After an exposure period of six months, tensile tests were conducted on the GFRP bars to determine the tensile properties of the exposed bars. A total of six beams were cast including three beams reinforced with the GFRP bars under direct sunlight only, and three beams reinforced with the GFRP bars subject to direct sunlight and seawater. The beams were then tested in flexure under two-point loading up to failure. LVDTs were used to measure crack widths of the beams, and strain gauges mounted on the GFRP bars were used to measure the strain in the bars.

[2] **Mohammad Adil Dar (2018)** in this paper we study was able to successfully test and validate the feasibility of using expanded polystyrene and timber in various CFS composite beams through experimental testing. The prominent results obtained in this study are highlighted as under: Initially a low cost innovative stiffening arrangement against premature buckling was attempted using high density expanded polystyrene as packing to fill the hollow space within the proposed innovative box compression flange. However, the local buckling failure on top face of box compression flange was observed at much lower load thus failed to produce expected results. Replacement of softer expanded polystyrene by wooden pads, at vulnerable spots (i.e., under concentrated applied load points), results in to much improved load carrying capacity from 27.3 kN (Model B) to 42.5 kN (Model C) (i.e., increase in strength by 55%). This confirms the importance of proper application of stiffening arrangements in CFS composite beam sections

[3] **B. Alfarah (2017)** in this paper we are studied behavior of reinforced concrete (RC) structures under severe demands, as strong ground motions, is highly complex; this is mainly due to joint operation of concrete and steel, with several coupled failure modes. Furthermore, given the increasing awareness and concern for the important seismic worldwide risk, new developments have arisen in earthquake engineering. Nonetheless, simplified numerical models are widely used (given their moderate computational cost), and many developments rely mainly on them. The authors have started a long-term research whose final objective is to provide, by using advanced numerical models, solid basis for these developments. Those models are based on continuum mechanics, and consider Plastic Damage Model to simulate concrete behavior. Within this context, this paper presents a new methodology to calculate damage variables evolution; the proposed approach is based in the Lubliner/Lee/Fenves formulation and provides closed-form expressions of the compressive and tensile damage variables in terms of the corresponding strains.

[4]Liu (2017) investigated the effect of variation of aspect ratio on the behaviour of concrete filled cold formed steel elliptical sections. A total of 21 stub columns including 3 axially loaded elliptical hollow sections was tested with an aspect ratio from 1 to 2.5 and the steel tube area to concrete area ratio varied from 5% to 12%. The height of all columns was taken as four times the major axis outer radius of the ellipse to ensure short column behaviour. The elliptical steel tubes were made from cold formed steel of 2.75 mm nominal thickness and were completed by seam welding. The elliptical hollow section specimens subject to concentric loading failed by local buckling. The concrete-filled columns failed by shear of the infill concrete

[5] Pallares and Hajjar (2010), Prakash et al. (2012) modified push tests to investigate the resistance and deformation capacity of shear connectors and studied the shear characteristics between concrete and steel sections. Hanaor (2002) presented several forms of shear connectors between light weight steel and concrete, and investigated these systems by push-out test and full scale composite element tests. Large scale composite slab specimens and push out tests were investigated by Lakkavalli and Liu (2006). Loading was applied at one third span points through a distribution beam loaded at mid point. This generated a constant moment region at the center part of the span..

IV. RESEARCH GAP

The approach to the design of cold formed sections in compression and bending that take account of local buckling of the thin steel sections and other member buckling modes, which may not occur in hot rolled steel sections. The design approach is based on BS EN 1993-1-3: Design of Steel Structures: Part 1.3: General Rules – Supplementary Rules for Cold Formed Members and Sheeting, 2006. Existing research information on composite beams using light steel sections and various forms of shear connector systems and composite columns using light steel sections.

OBJECTIVES

The first research task was to identify the forms of light steel composite beams that should be investigated by tests, FE modelling and practical evaluations. Two forms of construction were identified in order to understand the basic structural behaviour. These were: Perform bending tests on beams with different forms of lightweight shear connection systems to evaluate the degree of composite action that can be achieved. Finite element modeling of composite cold formed steel and concrete. Adapt the shear connection system to be able to optimize the performance for the minimum degree of composite action. Develop a calculation procedure consistent with the composite design principles of Eurocode but applying to light steel framing. This will consider both the cross-sectional resistance and stiffness for partial shear connection.

METHODOLOGY

- Establishing the current state of the art, particularly on shear connection systems applied to light steel framing and on composite columns.
- Defining and setting up tests aimed at investigating modes of failure and at determining the shear resistance and stiffness of new shear connector systems applied to light steel beams and columns.
- Correlating the tests with finite element models using ABAQUS in order to understand the failure modes and to extend the test information into a wider range of cases with suitable limitations.
- Developing design models based on evidence from the tests and presenting the models in accordance with the general principles of composite design.
- Discussing and preparing a tentative construction process for the developed systems that may be taken forward into practical application.

V. TEST PROGRAMME DESCRIPTION

All the tests carried out by using INSTRON universal testing machines at the laboratory of the University. For the beam tests, the test machine with 600 kN capacity was used and 1000 kN for the long columns tests. Short columns and slips tests were tested using an AVERY 1000 kN compression test machine.

All the beams were cast using cleaned galvanised steel C-sections and were tested as simply supported members subject to a single central point load. The load was transferred from a 70x100 mm steel plate placed to avoid concrete crushing under the point load. The top of the beams was levelled under the load plate to ensure uniform distribution of the load to the sections and the load was applied at the mid-span of beam span to create constant shear zone in order to determine the shear transfer between the steel and concrete.

Linear variable displacement transducers (LVDTs) were placed to record the mid-span deflection and of both beam-ends to record the slip between concrete and C-section. These are shown in Figure 1 Figure 2 shows a typical composite beam test with the load application at mid-span.

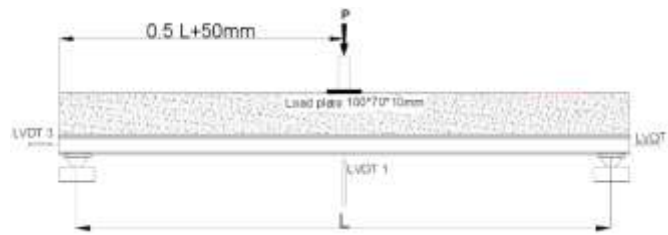


Figure 1: Typical test of composite beam using C-section as reinforcement

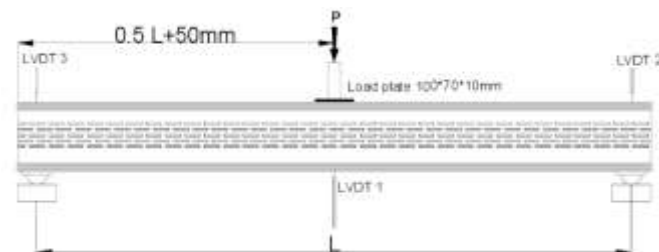


Figure 2: Test of steel C-section beam

ADAVANTAGES

- In this project does not consider the fire resistance of the proposed system, which will require additional reinforcement or board protection.
- Research on composite walls using cold formed steel and concrete using C-sections is required including the effect of concrete pressures during construction.
- The shear connection of the beams can be further improved by using screws and bolts with thicker C-sections. The tests showed that the spacing between connectors did not make a significant improvement in shear-bond strength.
- Testing composite cold formed members using different types of loading and continuous support conditions to provide a better understanding of the behaviour also under impact load.

CONCUSION

Light steel framing is widely used in low and medium-rise buildings but is limited in applications where longer spans and heavier loadings are required. Although composite action between steel and concrete is used in structural steel frames, the application of composite construction in light steel framing is relatively new, because suitable shear connection systems have not been developed.

In this project, a new form of light steel construction has been developed that uses C-sections as the effective tension and shear reinforcement and also as the encasement to concrete beam and columns. The shear connection system may be in the form of screws or bolts or perforations rolled into the C-sections. In this new form of construction, the C-sections support the concrete during the construction phase and also act compositely with the concrete to resist subsequent imposed loads. The light steel composite beams have a wide range of application by varying the depth of the side C-sections and can achieve spans up to 8m and loadings up to 5 kN/m².

The composite cross-section may be assumed to be cracked at the serviceability limit state and the plastic bending resistance may be used at the ultimate limit state. The longitudinal shear resistance is considered to be developed on the horizontal plane between the steel and concrete, which is analogous to the shear-bond behaviour in composite floor slabs.

REFERENCES

- [1] Abdel-Sayed G. (1982) 'Composite cold-formed steel-concrete beams', J Struct Div, Am Soc Civ Eng, 108 (ST11), pp 2609-22.
 Abdel-Sayed G. (1982), 6th International Specialty Conference on Cold-Formed Steel Structure, Missouri University of Science and Technology, Nov. 16th, Scholars Mine.
 Abdel-Sayed G. and Kwok-Cheung C. (1986) 'Ultimate strength of composite cold-formed steel-concrete columns', IABSE reports, pp 331-338.

- [2] Suhad M.Abd (2018) 'Mechanical Properties of the Light Weight Foamed Concrete with Steel Fiber of Different Aspect Ratio', 2018 1st International Scientific Conference of Engineering Sciences - 3rd Scientific Conference of Engineering Science (ISCES).
- [3] Farid Abed (2019) 'Effect of Harsh Environmental Conditions on the Bond-Dependent Coefficient of GFRP Bars in Concrete Beams' .
- [4]K. Alenezi a , M.M. Tahir a,† , T. Alhajri a , M.R.K. Badr b , J. Mirza (2015) 'Behavior of shear connectors in composite column of cold-formed steel with lipped C-channel assembled with ferro-cement jacket' , 0950-0618/2015 Elsevier Ltd.
- [5] Suparna Havelia(2020) 'Study And Analysis Of Variation In Behavior Of Mechanical Properties Of Carbon Powder Reinforced Concrete To Conventional Concrete' , 2020 International Conference on Intelligent Engineering and Management (ICIEM)
Ahmed A. (2014) 'Modelling of a reinforced concrete beam subjected to impact vibration using ABAQUS', International Journal of Civil and Structural Engineering, Vol. 4 (3), pp 227-236.
- [6] Alenezi K., Tahir M. M., Alhajri T., Badr M. R. K. and Mirza J. (2015) 'Behavior of shear connectors in composite column of cold formed steel with lipped C channel assembled with ferro-cement jacket', ELSEVIER, Constructional and Building Materials, 84 pp 39-45.
- [7] Alfarah B., Almansa F. L., and Oller S. (2017) 'New methodology for calculating damage variables evolution in Plastic Damage Model for RC Structures', ELSEVIER, Engineering Structures, 132, pp 70-86.
- [8] Bamga, S. O. et al. (2013) 'Feasibility of developing composite action between concrete and cold-formed steel beam, Springer, Journal of Central South University, 20, pp 3689-3696.
- [9] Baskar K. J., Arvinth A, Elahi A. A., Mohanraj B. and Parakash A. (2016) 'Experimental study on behaviour of cold formed steel using C channel section under axial compression', International Journal for Innovative Research in Science and Technology, Vol. 2 (11) pp 193-197.
- [10] Bouafia, Y. et al. (2014), 11th World Congress on Computational Mechanics/Stress-strain relationship for the confined concrete, IACM and ECCOMAS, Barcelona, Spain, 20-25 July, ASCE.
- [11] Dar M. A., Subramanian N., Anbarasu M. Dar A. R. and Jamaes B.P. (2018) 'Structural performance of cold-formed steel composite beams', Steel and Composite Structures, Vol. 27, No. 5, 545-554.
- [12] Dujmovic D., Androic B., Tonis D. and Lukacevic L. (2017) 'Composite columns made of concrete-filled hollow steel sections with embedded steel cores', Grdevinnar, 69(4), pp 295-306.
Dundu M. (2014) 'Buckling of short cold-formed lipped channels in compression', Journal of the South African Institution of Civil Engineering, Vol.56 (2), pp 46-53.
- [13] Evirgen B., Tuncan A., and Taskin K. (2014) 'Structural behaviour of concrete filled steel tubular sections(CFT/CFSt) under axial compression ', ELSEVIER, Journal of Thin Walled Structures, 80 pp 46-56.
- [14] Ferhoune M. (2014) 'Experimental behaviour of cold-formed steel welded tube filled with concrete made of crushed crystallized slag to eccentric load', ELSEVIER, Thin Walled Structures, 80 pp 159-166.
- [15] Goh W. I., Mohamad N., Abdullah R., Samad A. (2014) 'Compression test and finite element analysis of formed concrete cube', Journal of Engineering and Technology (JET), Vol. 5(1), pp.1-9
- [16] Hsu C. T., Punurai S., Punurai W. and Majdi Y. (2014) 'New composite beams having cold-formed steel joists and concrete slab', ELSEVIER, Engineering Structures, 71, pp 187-200.